

LT8610 AC TID TEST REPORT

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2. INTRODUCTION

The aim of this test campaign is to evaluate the Total Ionizing Dose (TID) radiation hardness level of the LT8610AC buck converter component.

The component is selected from an ESA internal list of Commercial of-the-shelf (COTS) components, which contains components of high importance for ESA projects. The results can then be used for the different projects. Additionally, the data is used to derive information on the general TID response of this device.

3. ACRONYMS

4. DEVICES UNDER TEST

In [Table 1](#page-4-1) the parameters of the Device Under Test (DUT) are given.

Table 1: Description of the DUT

This device is a synchronous buck converter with a half bridge configuration which is used to step down a voltage with a switching application. For the device a specific application close to

the usual application, as presented in the datasheet, was developed. In [Figure 1,](#page-5-0) a usual application for this synchronous buck converter with the internal MOSFETs (LDMOS) is given.

Figure 1: Typical application synchronous buck converter

In [Figure 2](#page-5-1) the Block diagram of the device is shown and in [Figure 3](#page-6-0) the decapsulated die can be seen.

Figure 2: Block Diagram of the LT8610

Figure 3:Microscope Picture of a decapsulated LT8610 (left) and the package (right)

5. TID SUMMARY

Table 2: TID Summary

6. DOSIMETRY AND IRRADIATION FACILITY

IRRADIATION FACILITY

Dose rate (rad(Si)/h): 350-360

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Conditions:

- Room Temperature Annealing (RTA) 21°C, 168 h
	- o Biased for those tested biased
	- o Unbiased for those tested unbiased
- High Temperature Annealing (Ageing) 100°C, 168 h
	- o Biased for those tested biased
	- o Unbiased for those tested unbiased

Values are provided in TID(H20), the conversion to TID(Si) is done using the conversion factor of: 0.898.

7. TEST PREPARATION

7.1. Test set-up

The test was performed at the Co-60 facility at ESTEC. The irradiation was performed in room temperature condition. For the test, the following equipment, [Table 3,](#page-8-0) was used:

Table 3: Test Equipment

In **Error! Reference source not found.** the basic test setup with the equipment and the test boards is visualized. Multiple different buck converters have been tested during the campaign. One of the test boards consist of the COTS LT8610.

In [Figure 4](#page-9-0) the DUT board can be seen. This board is then mounted on the radiation-test-board in Figure 5. Specific values for the capacitances and inductances were calculated for each board. The biasing can flexibly be adjusted by jumpers and relays. The relays can be used to switch measurements between the DUTs. In addition, the parameters of the device can be measured individually, and the device can be enabled and disabled. The relays are controlled outside the chamber with a specific designed relay-control-board.

In [Figure 6](#page-10-2) an overview with the important capacitances is given. The value of the output capacitance is calculated to Cout = 80 μ F, the input capacitance is Cin = 30 μ F the output Inductance is Lout = 4.2μ H.

Figure 4: Visualization of the radiation-test-boards

Figure 5: Top-side (left) and bottom-side (right) of the LT8610 test board

Figure 6: Simplified test setup with Cout = 80 µF, Cin = 30 µF, Lout = 4.2 µH.

7.2. Measurement

As stated above, the use of relays allows an individual measurement for each DUT on the radiation-test-boards. All-important measurable device parameters are provided in [Table 4.](#page-10-1)

Table 4: Measurement Parameters

7.3. Biasing Conditions

Two biasing conditions have been chosen and are displayed in Table 5.

Table 5: Test Conditions and description

Condition	Description
Unbiased	All pins shorted together; no pins left floating
Biased	Input voltage = 15 V, Frequency = 400 kHz, Output voltage 3.85 V, Output resistor = 50 Ohm

7.4. Data acquisition

All the data was acquired and saved with an oscilloscope or a source meter. The data was then processed for three sigma calculations. The values of the TID have been calculated based on the dosimetry provided in chapter 5 and is calculated accordingly to the TID in silicon.

8. TID EFFECTS RESULTS

8.1. Output Voltage

The output voltage of the LT8610 was set prior to the test campaign via a voltage divider between the output and the FB pin of the device. During the irradiation procedure no change in the output voltage was measured. In Figure 7 and Figure 8 the results of the campaign are displayed. Figure 7 shows the statistical analysis with the mean from the bias and unbiased configurations as well as the tolerance limits. The Upper Tolerance Limit (UTL) can be calculated as followed:

 $UTL = \delta_{\rm v} + K \cdot \sigma_{\rm v}$

with $\delta_{\rm x}$ the mean, K the one-sided tolerance limit factor, and σ the standard deviation. The lower tolerance limit (LTL) can be calculated with

 $LTL = \delta_{\rm x} - K \cdot \sigma_{\rm x}$. . 1990 – Paul III – Pa
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For the given P and C, the K value is 5.311 for n = 3 and 3.4 for n = 5. **Error! Reference source not found.**

Figure 7 shows the absolute values during the TID test campaign.

Figure 7: LT8610 relative output voltage change (Vout(pre-rad)/Vout(TID)) with the Room Temperature Annealing (RTA) and Accelerated Ageing for two bias conditions with tolerance limits for different TIDs in krad(Si)

Figure 8: LT8610 output voltage with the Room Temperature Annealing (RTA) and Accelerated Ageing for two bias conditions with tolerance limits for different TIDs in krad(Si)

9.1. VCC

The VCC voltage is the output voltage of the internal LDO used to supply the internal circuitry. An external capacitor is attached to flatten this voltage. During the irradiation period no change in the VCC was observed. Also, during measurements with the oscilloscope, a steady voltage without any ripples have been observed and is shown in Figure 9.

LT8610 Vcc at different TID levels

Figure 9: LT8610 Vcc voltage with the Room Temperature Annealing and Accelerated Ageing for two bias conditions

9.2. Shutdown quiescent current

The shutdown quiescent current is the current that is supplying the internal circuitry in the case of a shutdown of the device when the enable pin is connected to ground. The measured current was at a voltage of 15 V. A strong increase in the current after 30 krad was observed. The increase was close to 8 times the initial value. The results are shown in Figure 9 and Figure 10. The maximum variation given in the datasheet is well above the maximum limit measured.

Figure 10: LT8610 relative change in the shutdown quiescent current (Iq(pre-rad)/Iq(TID)) with the Room Temperature Annealing (RTA) and Accelerated Ageing for two bias conditions with tolerance limits for different TIDs in krad(Si)

LT8610 shutdown quiescent current at different TID levels

Figure 11: LT8610 shutdown quiescent current change of the LT8610 with displayed for two bias conditions

9.3. Frequency

The second parameter is the frequency. The frequency changed from around 400 to around 410 kHz, which will have a slight impact on the efficiency and the output ripple of the device. No difference between biased and unbiased group have been observed. Figure 11 and Figure Page 15/20 THE EUROPEAN SPACE AGENCY

12 displays the results. The change is below 6 %. There is no maximum variation given in the datasheet so no information if the frequency exceeds the limits can be given.

Figure 12: LT8610 relative output voltage change (Freq(pre-rad)/Freq(TID)) with the Room Temperature Annealing (RTA) and Accelerated Ageing for two bias conditions with tolerance limits for different TIDs in krad(Si)

Figure 13: LT8610 output voltage with the Room Temperature Annealing and Accelerated Ageing for two bias conditions

10. CONCLUSION

The LT8610 converter with the date code HY29 has been tested against Total Ionizing Dose effects. Two biasing conditions have been tested. For the biased condition three DUTs have been used and for the unbiased condition (all pins shorted together) five devices have been used. For both conditions and to the maximum tested dose in silicon of 38 krad, no critical drift outside of the datasheet values have been observed. Full functionality is given to that dose. No rebound effect was observed. In Table 2 a summary is given.

The data provided in the report should be handled with caution considering traceability challenges in the use of COTS. However, the data gives an overview of different kinds of TID effects and allows preparation for validation test campaigns and be able to identify possible mitigation techniques.

Table 6: TID Summary

11. REFERENCES

- [1] Analog Devices, 42V, 2.5A Synchronous Step-Down Regulator with 2.5µA Quiescent Current, Rev. B. 2021 Device, LT8610, [LT8610 \(Rev. B\) \(analog.com\)](https://www.analog.com/media/en/technical-documentation/data-sheets/lt8610.pdf)
- [2] ESA-ESTEC (2012). "Space product assurance, Radiation hardness assurance EEE components, ECSS-Q-ST-60-15C"

12. ANNEX

In the following tables the values of the measurements are displayed. Sample number 1-3 are biased samples, Sample number 4-9 are the unbiased samples.

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